

Effect of aspect ratio on basic-flow pattern induced by thermocapillary effect in free liquid film

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Background

Thermocapillary-driven flow is realized by a surface tension difference due to non-uniform temperature distribution over the free surface. The fluid on the surface is generally driven from a region at higher temperature to that at lower temperature. Dr. Donald Roy Pettit, a NASA astronaut, demonstrated a series of experiments in the International Space Station in 2003 [1]. In this experiment, he formed a thin free liquid film of water in a metallic ring and placed a heated iron close to one side of the ring. From this experiment, he found that the fluid was driven from a colder region to a hotter region even though the fluid has a negative temperature coefficient of surface tension. After such unique demonstrations, Ueno and Torii [2] indicated there exist two major basic flows in a free liquid film; double-layered flow (DLF) and single-layered flow (SLF). The mechanism and selection of basic flows are discussed by numerical simulation [3-5], but little discussion has been done by experimental investigations except Fei et al. [6].

In the present study, we focus on a multicellular flow structures in single-layered flow (SLF) by changing Γ_{zx} . In our experiments, a liquid film of 6-cSt silicone oil ($Pr = 83.25$) is formed in a rectangular hole in the aluminum plate. We discuss the **formation of the multicellular structures** by making comparisons with numerical results.

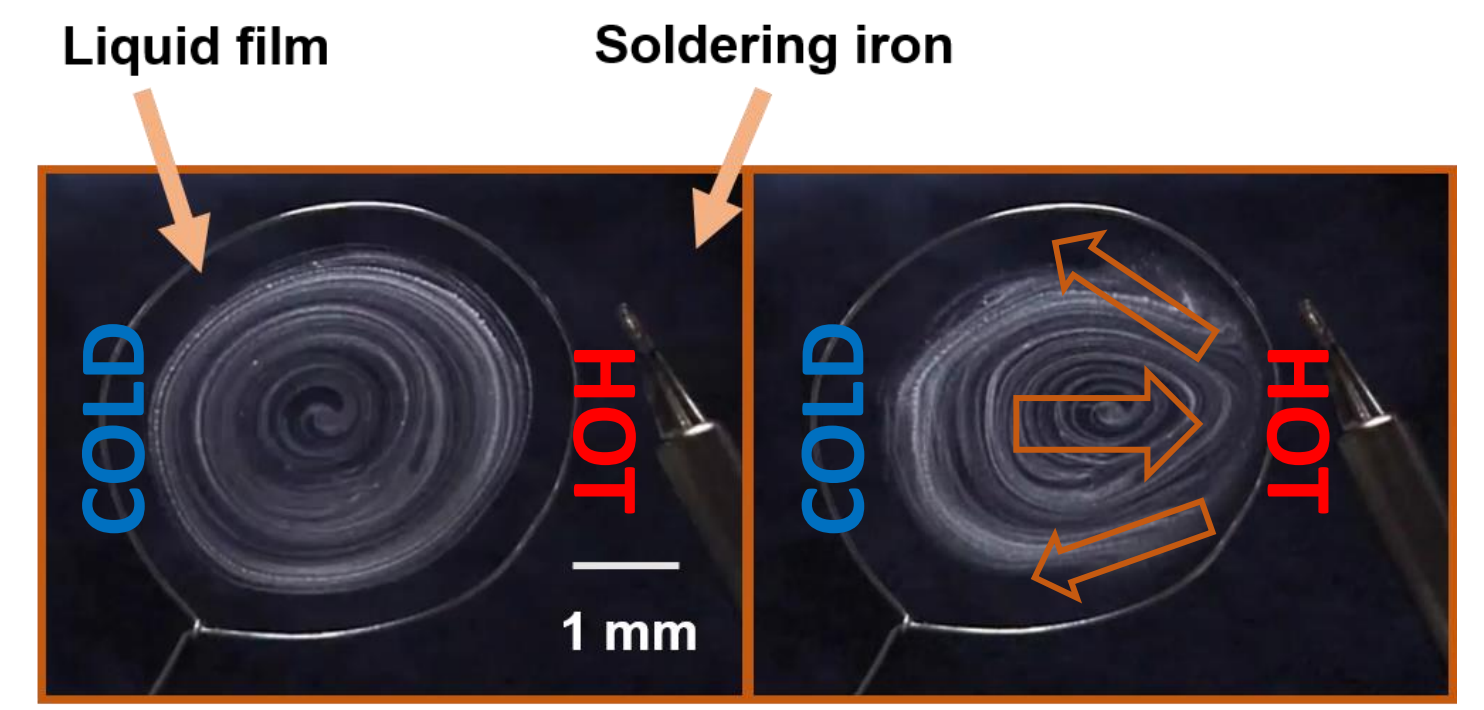


Fig. 1 Experiment on the ISS by Dr. Donald Roy Pettit in 2003 (©NASA). The fluid was driven from a colder region to a hotter region.

Symbols

Nomenclatures

D_p	diameter of tracer particle	[m]
d	depth of the film	[mm]
L_x	end-wall distance	[mm]
L_z	span-wise length	[mm]
T	temp.	[°C]
T_c	temp. at cold side	[°C]
T_h	temp. at hot side	[°C]
u	velocity of x component	[m/s]
x	position in streamwise direction	[-]
y	position in depth direction	[-]
z	position in spanwise direction	[-]
V	liquid volume	[m ³]
V_0	volume of hole region	[m ³]
Geeks		
ΔT	temp. difference	[°C]
κ	thermal diffusivity of fluid	[m ² /s]
μ	viscosity of fluid	[Pa s]
ν	kinetic viscosity of fluid	[m ² /s]
ρ	density of fluid	[kg/m ³]
ρ_p	density of particle	[kg/m ³]
σ_T	temp. coefficient of surface tension	[N/(m K)]

Experimental apparatus

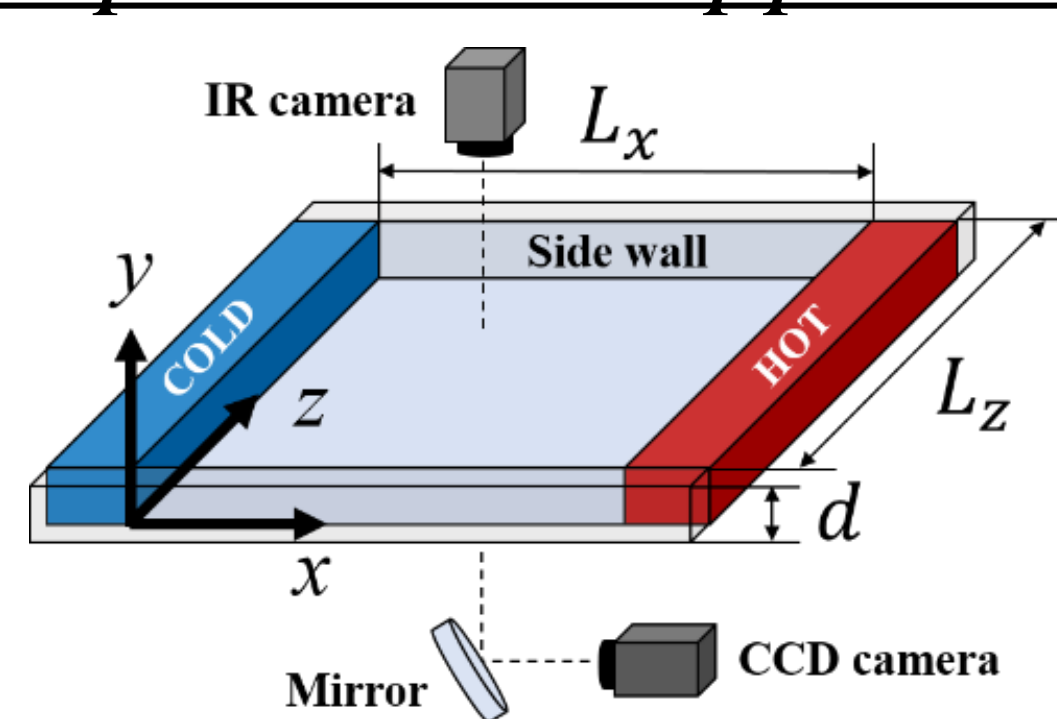


Fig. 2 Schematic of experimental apparatus. Temperature is taken by IR camera and the convection is taken by CCD camera.

Experimental conditions

Non-dimensional numbers

- Aspect ratio
 $\Gamma_{zx} = L_z/L_x$
- Stokes number
 $St = \frac{\rho_p D_p^2 u}{18\mu d}$
 $= 0 (10^{-5} \sim 10^{-4})$
- Marangoni number
 $Ma_L = \frac{|\sigma_T| (\Delta T/L_x) d^2}{\rho\nu\kappa}$

Properties

• Test fluid [7]

6-cSt silicon oil (at 25 °C)		
Prandtl number	[-]	83.25
Density	[kg/m ³]	916
Kinetic viscosity	[m ² /s]	6.0×10^{-6}
Thermal diffusivity	[m ² /s]	7.31×10^{-8}
Thermal expansion coefficient	[1/K]	1.09×10^{-3}
Surface tension	[N/m]	1.98×10^{-2}
Temp. coeff. of surface tension	[W/(m K)]	-5.79×10^{-5}

• Tracer particle

Gold-coated acrylic particle	
Diameter [μm]	15
True specific gravity [-]	1.80

• Test plate

Material of the plate	Aluminum
Thermal conductivity [W/(m K)]	236
Thermal diffusivity [m ² /s]	97.4×10^{-6}

Results (Experiment)

Cell number in SLF of the free liquid film with L_z (span-wise length)

flow field and temp. distribution over free surface	Ma_L (ΔT [K])	cell # (pair)
(a)	25 (4.3)	1(2)
(b)	34 (10)	2(4)
(c)	47 (9.4)	3(6)
(d)	52 (15)	4(8)

Fig. 4 Flow and temp. filed over free surface. Each (L_x, d, L_z) [mm] are (a)(1.0, 0.3, 6.0), (b)(1.0, 0.3, 9.0), (c)(1.0, 0.3, 12.0), (d)(1.0, 0.3, 18.0).

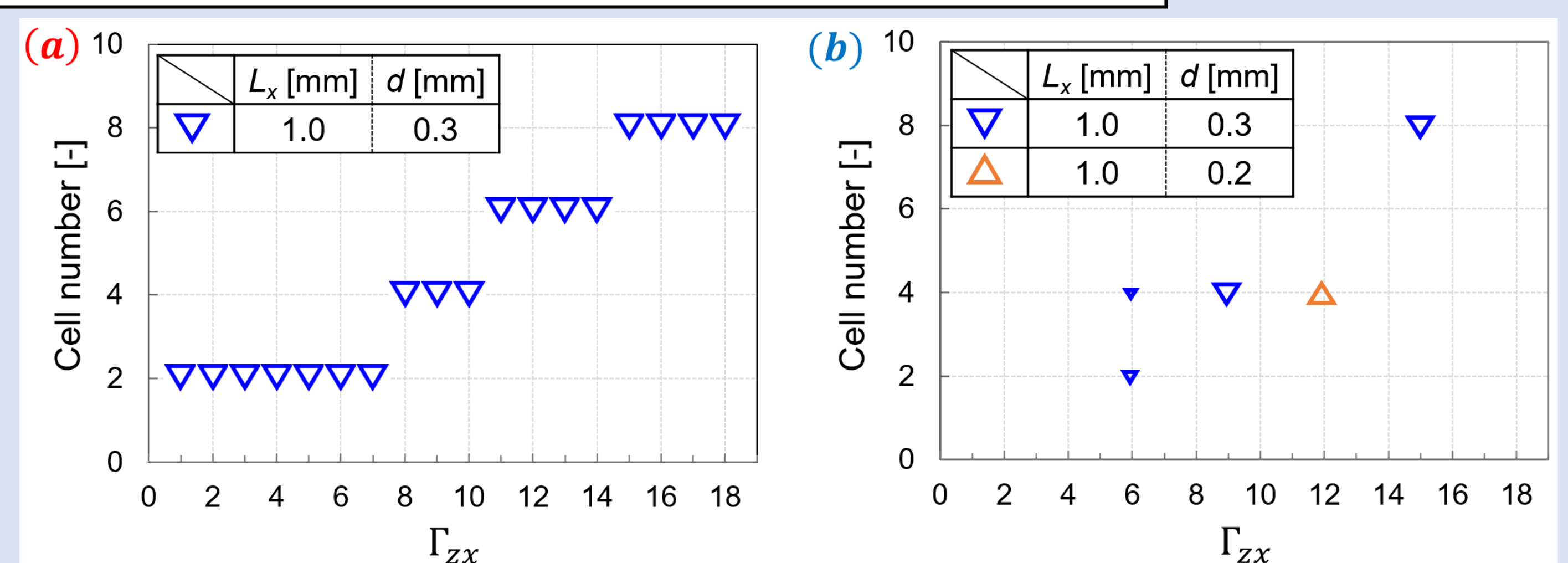


Fig. 5 Number of cell visualized over free surface of the film with Γ_{zx} . (a) is $V/V_0 = 0.9$, (b) is $V/V_0 = 0.75$.

- ▶ Figure 4 shows cell number of SLF is increased as the increase of span-wise length (which means, the structure of SLF flow is depends on aspect ratio of free liquid film).
- ▶ Figure 5 indicates cell number changes as aspect ratio to a threshold (ex. $\Gamma_{zx} = 8, 13, 15$).
- ▶ In the experiment up to now, the change of the cell structure has been confirmed even in the free liquid film with different volume ratio ($V/V_0 = 0.9$ and $V/V_0 = 0.75$).

Cell size variation

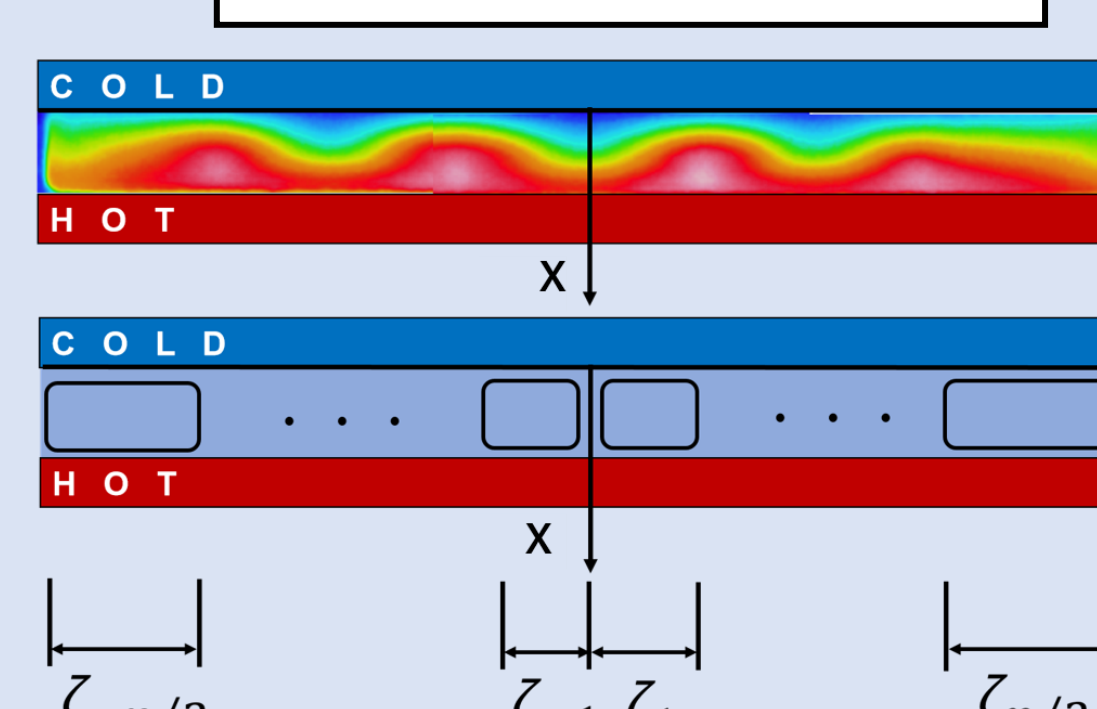


Fig. 6 Definition of cell length (ζ).

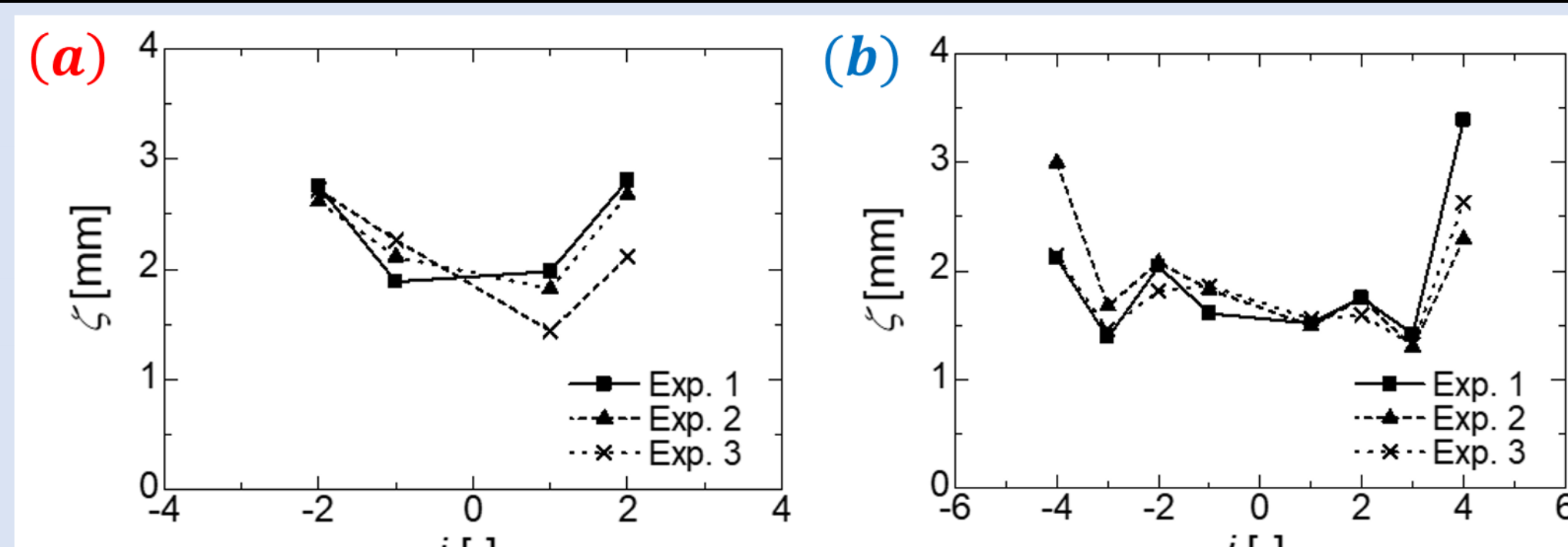


Fig. 7 Number of cell visualized over free surface of the film with Γ_{zx} . (a) is (1.0, 0.3, 9.0), (b) is (1.0, 0.3, 18.0).

- ▶ In order to quantitatively evaluate each cell in SLF, each cell is defined as shown in Fig. 6.
- ▶ It is found that the size of the cells in the central region is almost constant and smaller than those near the side walls ($n \geq 4$).

Results (Numerical simulation)

- ▶ Numerical simulations also show that the number of cells increases from two to four when $\Gamma_{zx} \geq 4$. However, unlike experiments, no further increase has been confirmed until now.
- ▶ The flow from the cross-section direction ($x - y$) observed in the numerical calculation is different from the experiment (Fei et al.).

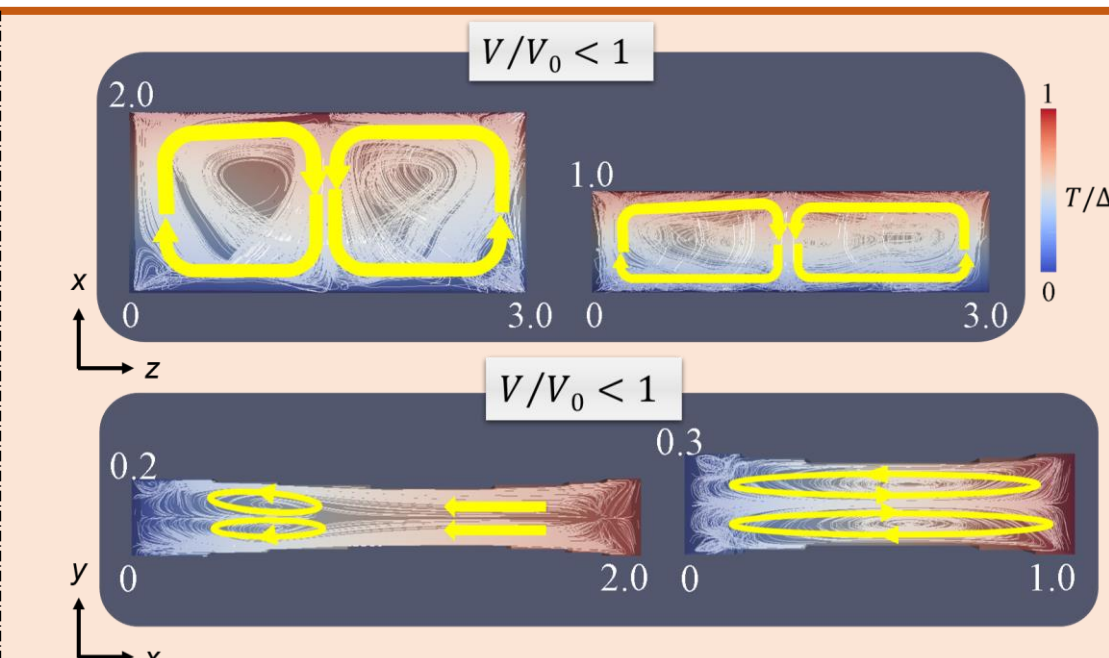


Fig. 8 Convection field and temperature field by numerical simulation of free liquid film (2.0, 0.2, 3.0) and (1.0, 0.3, 3.0).

Summary

- ▶ Multicellular structures induced by the thermocapillary effect in the free liquid films are investigated experimentally and numerically. Correlation between the cell number/size and the liquid-film aspect ratio is illustrated.
- ▶ The size of cells expressed in SLF varies in location.

Future plans

- ▶ General criteria for the pattern formation in the free liquid film and its occurring condition will be indicated, and will be compared to those of such as Rayleigh-Bénard and Marangoni-Bénard convections.
- ▶ Effects of bottom walls on the thermocapillary-driven convection and pattern formation will be discussed taking account of the thermal-flow fields and the energy analysis.

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